

# Model Predictions of Latitude-Dependent Ozone Depletion Due to Supersonic Transport Operations

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Results are presented from a two-dimensional model of the stratosphere that simulates the seasonal movement of ozone by both wind and eddy transport, and contains all the chemistry known to be important. The calculated reductions in ozone due to NO<sub>2</sub> injection from a fleet of supersonic transports are compared with the zonally averaged results of a three-dimensional model for a similar episode of injection. The agreement is good in the northern hemisphere, but is not as good in the southern hemisphere. Both sets of calculations show a strong corridor effect in that the predicted ozone depletions are largest to the north of the flight corridor for aircraft operating in the northern hemisphere.

## Introduction

CALCULATIONS by previous workers such as Johnston,<sup>1</sup> McElroy et al.,<sup>2</sup> Crutzen,<sup>3</sup> and Whitten et al.<sup>4</sup> have shown that the operation of aerospace vehicles in the Earth's stratosphere can be expected to deplete the Earth's ozone layer. The majority of these calculations are based on one-dimensional models that do not simulate the horizontal movement of ozone and other tracers by winds. Hence, the models cannot be used to calculate the latitude dependence of the ozone depletion.

Recently, preliminary calculations have become available from models<sup>5-8</sup> that do simulate the transport of ozone by winds. However, because these models are still in the developmental stage, each model as yet has not included some important factor, such as seasonal transport, nitric-acid chemistry, or the simultaneous solution of the odd-oxygen/odd-nitrogen chemical systems.

This paper presents results from a two-dimensional model that simulates seasonal transport of ozone by winds and contains all the chemistry presently known to be important. Comparisons of model predictions with experimental measurements for the spread of a radioactive tracer from nuclear tests are presented as well as the model predictions for the perturbations in the stratosphere caused by aerospace vehicles.

## The Model

The model is based upon the governing equations for trace constituents

$$(\partial n_i / \partial t) + \nabla \cdot n_i v + \Phi_i = Q_i \quad (1)$$

$$\Phi_i = -K_e \left[ \nabla n_i + \left( \frac{1}{H} + \frac{1}{T} \frac{dT}{dz} \right) n_i \hat{e}_z \right] \quad (2)$$

in which  $n_i$  and  $\Phi_i$  are the concentration and flux, respectively, of the  $i^{\text{th}}$  constituent,  $Q_i$  is the respective chemical production and loss rate term,  $H$  and  $T$  are the atmospheric scale height and temperature,  $\hat{e}_z$  is a vertical unit vector,  $v$  is the bulk velocity of the atmosphere, and  $K_e$  is the eddy diffusivity tensor.

The chemical rate equations are solved using an implicit technique. Omitting the transport term from Eq. (1) yields the finite difference form

$$(n_i^{j+1} - n_i^j) / \Delta t = Q_i^{j+1} \quad (3)$$

which can be linearized by taking the first term in a Taylor series expansion of  $Q_i^{j+1}$  about  $Q_i^j$

$$\frac{n_i^{j+1} - n_i^j}{\Delta t} = Q_i^j + \sum_k \frac{\partial Q_i^j}{\partial n_k} (n_k^{j+1} - n_k^j) \quad (4)$$

The members of the set of mass conservation equations are coupled and require solution by matrix methods. With the implicit method, large time steps can be taken even though the equations are very stiff.

The transport computations are time-split into those for vertical and horizontal advection and diffusion. Solutions for the transport processes are obtained from a mass conserving, forward time, space-centered finite difference formulation of the equations. An implicit formulation is used for the horizontal diffusion and an explicit formulation is used for all other transport processes.

Spherical geometry is employed in Eqs. (1) and (2) with the horizontal coordinate extending along a meridian from 80°S to 80°N in 5° intervals and the vertical coordinate extending from the ground to 60 km in 2.5-km intervals (Fig. 1). End boundaries are taken at 80°S and 80°N because meridional fluxes are expected to be small at these latitudes. The end boundary conditions are taken to be zero flux of all constituents across the vertical boundaries. The upper boundary conditions are given by setting the vertical flux equal to zero for all species. The lower boundary condition for all species

Presented as Paper 76-176 at the AIAA 14th Aerospace Sciences Meeting, Washington, D. C., Jan 26-28, 1976; submitted Feb. 20, 1976; revision received Sept. 29, 1976.

Index category: Atmospheric, Space, and Oceanographic Sciences.

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Table 1 Reaction rate coefficients<sup>a</sup>

Number	Process	Reaction rate coefficient	Reference
1	$O + O_3 \rightarrow 2 O_2$	$1.9 \times 10^{-11} \exp(-2300/T)$	11
2	$O + O_2 + M \rightarrow O_3 + M$	$1.1 \times 10^{-34} \exp(510/T)$	12
3	$NO_2 + O \rightarrow NO + O_2$	$9.1 \times 10^{-12}$	13
4	$NO + O_3 \rightarrow NO_2 + O_2$	$9.0 \times 10^{-13} \exp(-1200/T)$	14
5	$NO_3 + NO \rightarrow 2 NO_2$	$2.0 \times 10^{-11}$	12
6	$O_3 + NO_2 \rightarrow NO_3 + O_2$	$6.3 \times 10^{-12} \exp(-3500/T)$	12
7	$O(^1D) + M \rightarrow O + M$	$5.4 \times 10^{-11}$	15
8	$O + OH \rightarrow H + O_2$	$4.2 \times 10^{-11}$	12
9	$O_3 + H \rightarrow OH + O_2$	$2.6 \times 10^{-11}$	12
10	$NO + O + M \rightarrow NO_2 + M$	$3.0 \times 10^{-33} \exp(940/T)$	16
11	$NO_2 + NO_3 + M \rightarrow N_2O_5 + M$		17 <sup>b</sup>
12	$O(^1D) + H_2O \rightarrow 2 OH$	$3.5 \times 10^{-10}$	14
13	$O_3 + HO_2 \rightarrow OH + 2 O_2$	$1.0 \times 10^{-13} \exp(-1250/T)$	12
14	$O + HO_2 \rightarrow OH + O_2$	$8.0 \times 10^{-11} \exp(-550/T)$	12
15	$NO_2 + OH + M \rightarrow HNO_3 + M$		17 <sup>b</sup>
16	$OH + HNO_3 \rightarrow H_2O + NO_3$	$6.0 \times 10^{-13} \exp(-400/T)$	12
17	$O + O + M \rightarrow O_2 + M$	$1.0 \times 10^{-32}$	12
18	$OH + HO_2 \rightarrow H_2O + O_2$	$6.0 \times 10^{-11}$	12
19	$OH + CO \rightarrow H + CO_2$	$1.36 \times 10^{-13}$	12
20	$H + O_2 + M \rightarrow HO_2 + M$	$6.7 \times 10^{-33} \exp(290/T)$	12
21	$O + HNO_3 \rightarrow OH + NO_3$	$1.5 \times 10^{-14}$	12
22	$OH + O_3 \rightarrow HO_2 + O_2$	$1.6 \times 10^{-12} \exp(-1000/T)$	11
23	$NO + HO_2 \rightarrow NO_2 + OH$	$2.0 \times 10^{-13}$	12
24	$NO_2 + O + M \rightarrow NO_3 + M$		17 <sup>b</sup>
25	$N_2O_5 + M \rightarrow NO_2 + NO_3 + M$		17 <sup>b</sup>
26	$H + OH + M \rightarrow H_2O + M$	$6.1 \times 10^{-26} T^{-1/2}$	12
27	$N + O_3 \rightarrow NO + O_2$	$5.7 \times 10^{-13}$	12
28	$N + NO \rightarrow N_2 + O$	$2.7 \times 10^{-11}$	12
29	$N + O_2 \rightarrow NO + O$	$1.1 \times 10^{-14} T \exp(-3150/T)$	12
30	$N + OH \rightarrow NO + H$	$5.7 \times 10^{-11}$	12
31	$NO + OH + M \rightarrow HNO_2 + M$	$2.2 \times 10^{-32} \exp(1100/T)$	12
32	$NO_2 + HO_2 \rightarrow HNO_2 + O_2$	$3.0 \times 10^{-14}$	12
33	$OH + HNO_2 \rightarrow H_2O + NO_2$	$1.3 \times 10^{-13}$	12
34	$O(^1D) + N_2 + M \rightarrow N_2O + M$	$2.8 \times 10^{-36}$	12
35	$O(^1D) + N_2O \rightarrow N_2 + O_2$	$1.1 \times 10^{-10}$	12
36	$O(^1D) + N_2O \rightarrow 2 NO$	$1.1 \times 10^{-10}$	12
37	$O + HNO_2 \rightarrow OH + NO_2$	$1.5 \times 10^{-14}$	12
38	$OH + OH + M \rightarrow H_2O_2 + M$	$2.5 \times 10^{-33} \exp(2550/T)$	12
39	$OH + H_2O_2 \rightarrow H_2O + HO_2$	$1.7 \times 10^{-11} \exp(-910/T)$	12
40	$HO_2 + HO_2 \rightarrow H_2O_2 + O_2$	$3.0 \times 10^{-11} \exp(-500/T)$	12
41	$O + H_2O_2 \rightarrow OH + HO_2$	$1.1 \times 10^{-12} \exp(-2125/T)$	18, 19 <sup>c</sup>
42	$O + H_2O_2 \rightarrow H_2O + O_2$	$1.6 \times 10^{-12} \exp(-2125/T)$	18, 19 <sup>c</sup>
43	$HCl + OH \rightarrow H_2O + Cl$	$2.8 \times 10^{-12} \exp(-400/T)$	20
44	$HCl + O \rightarrow OH + Cl$	$1.9 \times 10^{-11} \exp(-3573/T)$	21
45	$Cl + CH_4 \rightarrow HCl + CH_3$	$5.1 \times 10^{-11} \exp(-1790/T)$	21
46	$Cl + H_2 \rightarrow HCl + H$	$2.0 \times 10^{-11} \exp(-2164/T)$	21
47	$Cl + O_3 \rightarrow ClO + O_2$	$3.4 \times 10^{-11} \exp(-300/T)$	20
48	$ClO + O \rightarrow Cl + O_2$	$5.7 \times 10^{-11}$	21
49	$ClO + NO \rightarrow NO_2 + Cl$	$1.7 \times 10^{-11}$	21
50	$ClO + CO \rightarrow CO_2 + Cl$	$1.7 \times 10^{-15}$	21

<sup>a</sup>Units in  $\text{sec}^{-1}$  for unimolecular reactions,  $\text{cm}^3 \text{sec}^{-1}$  for bimolecular reactions,  $\text{cm}^6 \text{sec}^{-1}$  for termolecular reactions.

<sup>b</sup>The pressure-dependent rate constant is calculated using a three-level system and is fitted to available rate data at high, low, and intermediate pressures. Details are given in Turco and Whitten.<sup>17</sup>

<sup>c</sup>Values are based on the measurement of the total reaction rate of  $O$  and  $H_2O_2$  by Garvin and Hampson<sup>18</sup> and the ratio of the reaction rates for reactions 41 and 42 recommended by Nicolet.<sup>19</sup>

### Transport

The mean meridional circulation is obtained by the kinematic method from the averaged equation of mass continuity. With the assumption that the density field is in a steady state, the approximate form of this equation in spherical coordinates is

$$\frac{1}{R \cos \phi} \frac{\partial (\bar{\rho} \bar{v} \cos \phi)}{\partial \phi} + \frac{\partial (\bar{\rho} \bar{w})}{\partial z} = 0 \quad (5)$$

where the overbar denotes an average with respect to time and longitude,  $\bar{\rho}$  is the bulk density,  $\bar{v}$  and  $\bar{w}$  are the meridional and vertical velocity components,  $R$  is the radius of the earth, and  $\phi$  the latitude. Equation (5) implies the existence of a except  $HNO_3$ ,  $NO_2$ ,  $O_3$ ,  $N_2O$ ,  $HCl$ , and  $H_2O_2$  is chemical

Table 2 Photodissociation rates for O-H-N-Cl system (in units of  $\text{sec}^{-1}$  at zero optical depth)

Number	Process	Rate coefficient	Reference
J1	$O_2 + h\nu \rightarrow 2 O(^3P)$	$3.6 \times 10^{-6}$	22, 23, 24, 25
J2	$O_3 + h\nu \rightarrow O_2 + O(^3P)$	$5.6 \times 10^{-4}$	26, 27, 28
J3	$O_3 + h\nu \rightarrow O_2 + O(^1D)$	$9.6 \times 10^{-3}$	26, 27, 28
J4	$NO + h\nu \rightarrow N + O$	$1.4 \times 10^{-5}$	29
J5	$NO_2 + h\nu \rightarrow NO + O$	$1.0 \times 10^{-2}$	30, 31, 32
J6	$H_2O + h\nu \rightarrow OH + H$	$5.6 \times 10^{-6}$	33
J7	$HNO_3 + h\nu \rightarrow NO_2 + OH$	$1.4 \times 10^{-4}$	34, 35
J8	$HNO_2 + h\nu \rightarrow NO + OH$	$6.6 \times 10^{-4}$	36
J9	$N_2O + h\nu \rightarrow N_2 + O(^1D)$	$1.4 \times 10^{-6}$	37, 38, 39
J10	$NO_3 + h\nu \rightarrow NO_2 + O$	$2.55 \times 10^{-2}$	36
	$+ NO + O_2$	$4.08 \times 10^{-2}$	36
J11	$N_2O_5 + h\nu \rightarrow 2 NO_2 + O$	$6.0 \times 10^{-4}$	40
J12	$HO_2 + h\nu \rightarrow OH + O$	$1.0 \times 10^{-3}$	41
J13	$H_2O_2 + h\nu \rightarrow 2 OH$	$1.7 \times 10^{-4}$	42, 43
J14	$HCl + h\nu \rightarrow H + Cl$	$2.4 \times 10^{-5}$	44
J15	$ClO + h\nu \rightarrow O + Cl$	$4.5 \times 10^{-3}$	45

"stream function"  $\psi$  for the total mass flux such that

$$2\pi R \bar{\rho} \bar{v} \cos \phi = - \frac{\partial \psi}{\partial z} \quad 2\pi R \bar{\rho} \bar{w} \cos \phi = \frac{\partial \psi}{R \partial \phi} \quad (6)$$

If the distribution of  $\bar{\rho}$  and  $\bar{v}$  is known, the first of these can be integrated vertically, and  $\bar{w}$  can be obtained from the second.

Up to 20 km, the density was obtained from data presented by Oort and Rasmusson,<sup>46</sup> and above that altitude by vertical integration of the hydrostatic equation, using mean (rocket) temperatures.<sup>47</sup>

The  $\bar{v}$  components were based on the results<sup>46</sup> up to 20 km. These values were then extrapolated to the top of the model by imposition of a simple vertical profile that matched the 20-km value and satisfied the kinematic constraint that there be no equilibrium. Because  $HNO_3$ ,  $HCl$ , and  $H_2O_2$  are water soluble, their number densities are set equal to zero at the lower boundary. The number densities of  $NO_2$  and  $N_2O$  are fixed at  $3 \times 10^9 \text{ cm}^{-3}$  and  $7.5 \times 10^{12} \text{ cm}^{-3}$ , respectively, at the lower boundary while that of  $O_3$  is fixed at  $6 \times 10^{11} \text{ cm}^{-3}$  (see Ref. 9).

The chemistry employed in this model is a simplified version of that used in our one-dimensional model studies.<sup>10</sup> At each time step, the model calculates the concentrations of  $O_3$ ,  $O(^3P)$ ,  $O(^1D)$ ,  $NO_2$ ,  $NO$ ,  $NO_3$ ,  $N_2O$ ,  $N_2O_5$ ,  $HNO_3$ ,  $HNO_2$ ,  $H_2O_2$ ,  $HO_2$ ,  $N$ ,  $OH$ ,  $H$ ,  $Cl$ ,  $ClO$ , and  $HCl$ . The profiles of  $N_2$ ,  $O_2$ ,  $H_2O$ ,  $H_2$ ,  $CH_4$ ,  $CO$ , and  $CO_2$  are held fixed (at the experimentally determined values) during the calculations.

The rate coefficients are shown in Table 1, and the photolysis rates at zero optical depth are given in Table 2.

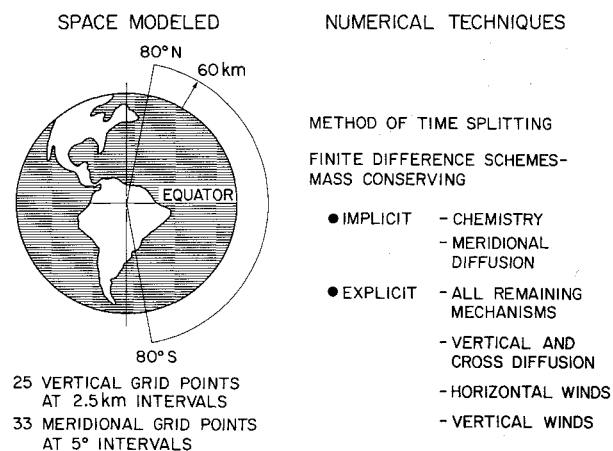


Fig. 1 Model geometry and techniques.

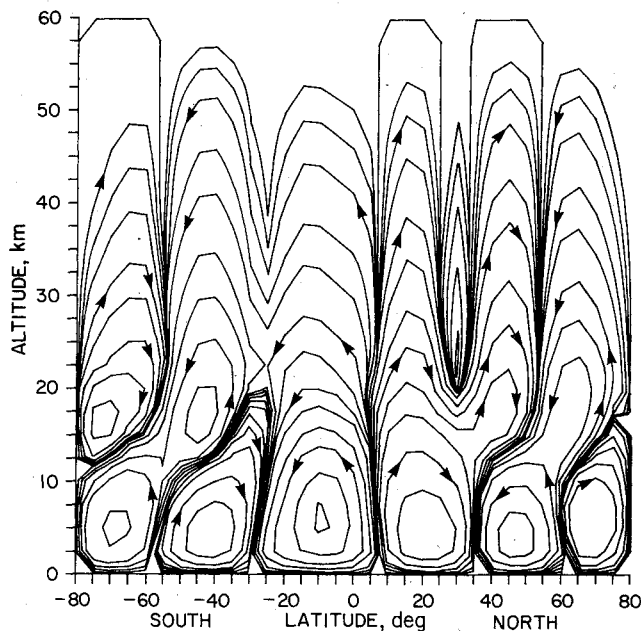


Fig. 2 Stream function; fall in the northern hemisphere.

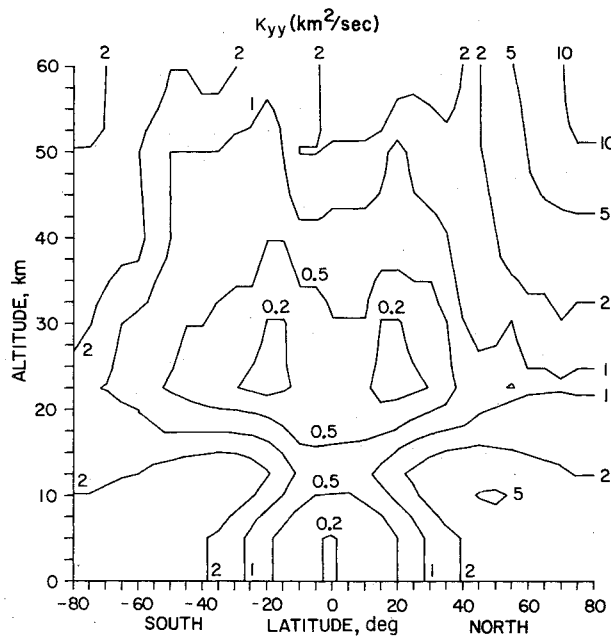


Fig. 3  $K_{yy}$ ; fall in the northern hemisphere.

net mass flux across any vertical latitude wall. This constraint arises because the model has a rigid top and bottom. In addition, a meridional variation was imposed that resulted in a three-cell circulation structure ( $80^\circ\text{N}$ – $80^\circ\text{S}$ ) in the stratosphere and lower mesosphere during the summer and winter seasons and four-cell structure in spring and fall. This should approximate the circulation patterns obtained by other investigators (e.g., Murgatroyd and Singleton,<sup>48</sup> Vincent<sup>49</sup>). The first segment of Eq. (6) was then integrated vertically with the condition that  $\psi=0$  on all boundaries. The resulting circulation patterns are reasonable in the troposphere and lower stratosphere (Fig. 2) but need further refinement in the upper portion of the model.

There are always uncertainties in the mean meridional circulation, even in the troposphere where sufficient wind data are available. Meridional wind speeds are generally less than 1 m/sec, except in the upper equatorial troposphere. Vertical wind speeds attain maxima in excess of 4 mm/sec in the equatorial troposphere; but are usually less than 1 mm/sec except in the vicinity of cell boundaries.

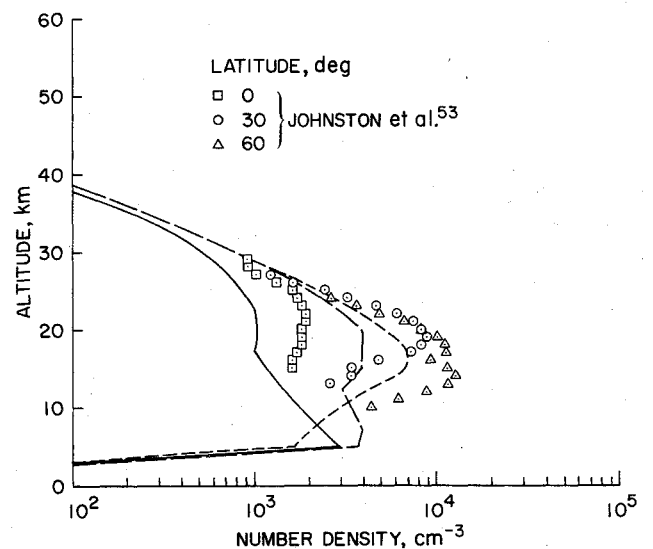


Fig. 4 Vertical distributions of carbon 14 at various latitudes. Experimental points are from Johnston et al.<sup>53</sup>

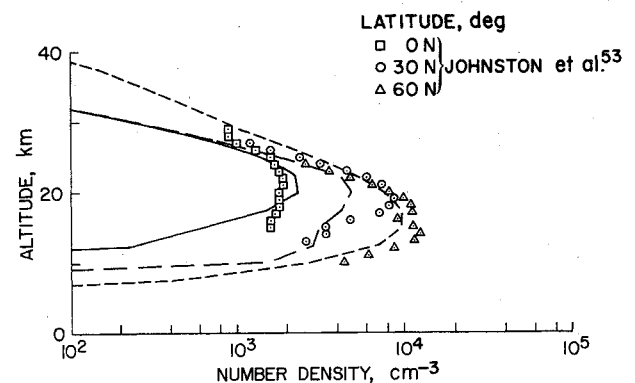


Fig. 5 Calculated vs predicted carbon 14 concentrations for the adjusted winds and transport coefficients of Louis.<sup>54</sup>

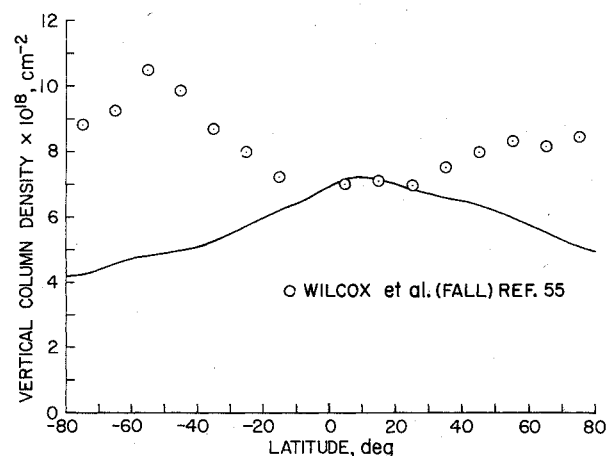


Fig. 6 Calculated vs predicted ozone column density as a function of latitude for the adjusted winds and transport coefficients of Louis.<sup>54</sup>

The eddy fluxes are modeled by diffusion coefficients based on the method of Reed and German.<sup>50</sup> The data of Luther<sup>51</sup> were used up to 20 km. These values were extended to the higher levels by assuming that  $K_{yy}$  is proportional to the variance of the  $v$  component, and that the slopes of the mixing surfaces are proportional to the slopes of the mean isentropic surfaces. Given  $K_{yy}$ , the other coefficients were obtained from (see Reed and German<sup>50</sup>)

$$K_{yz} = \bar{\alpha} K_{yy} \quad K_{zz} = (\bar{\alpha}^2 + \bar{\alpha}'^2) K_{yy} \quad (7)$$

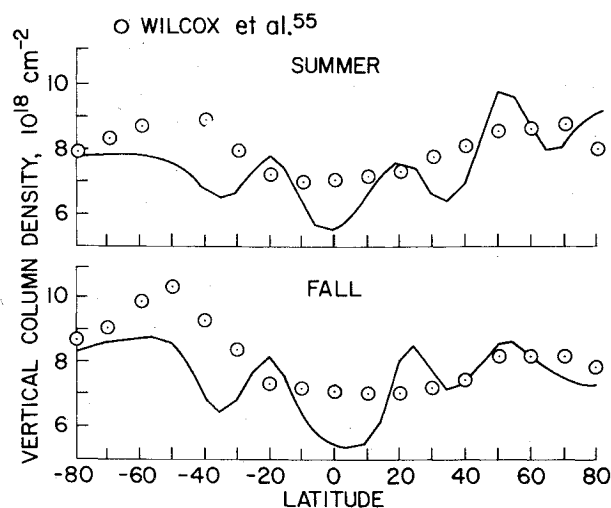


Fig. 7 Calculated vs predicted ozone column densities as a function of latitude for two seasons. The measurements were taken from Wilcox et al.<sup>55</sup>

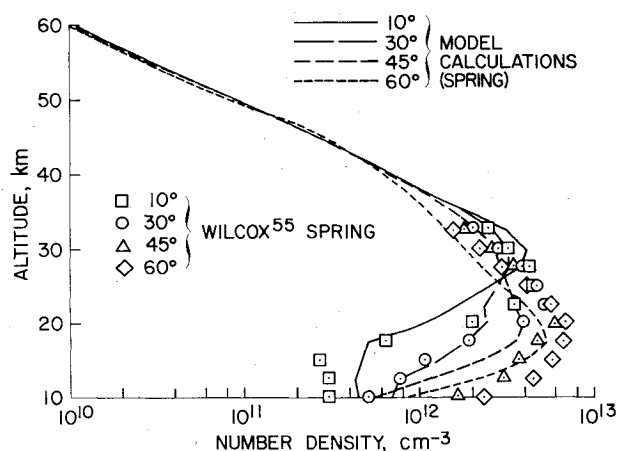


Fig. 8 Calculated vs predicted ozone concentration as a function of altitude for four different latitudes. Measurements are those of Wilcox et al.<sup>55</sup>

where  $\bar{\alpha}$  is the mean slope of the mixing surface, and  $\overline{\alpha'^2}$  its variance. The value of  $\overline{\alpha'^2}$  was assumed to be constant. The variances of  $v$  were taken from Nastrom et al.<sup>52</sup> Representative  $K_{yy}$  values are shown in Fig. 3.

### Results

Using the model described in the preceding sections, we have computed the spread of an inert radioactive tracer (carbon 14) from the 1963–1965 nuclear-test data presented by Johnston et al.<sup>53</sup> The model was started by using the Jan. 1963 data for the initial number densities and run for 1 year (i.e., 4 seasons). The results are presented as lines appropriate for 0°, 30°, and 60°N latitudes. The data points shown on Fig. 4 are the measured carbon 14 concentrations vs altitude for three latitudes for Jan. 1964. This figure shows that, although the calculated number densities follow the shape of the measured curves above 10 km, they are generally too low, sometimes by a factor of two. This implies that the calculated loss rate of the tracer is larger than observed and that calculations using the transport previously described tend to underestimate the residence time of any injected species.

Unfortunately, it is not sufficient to simply pick a set of seasonal winds and transport coefficients that result in a good prediction for the disappearance of carbon 14 with time. Figure 5 compares the predicted and measured carbon 14 concentrations when the transport coefficients of Louis<sup>54</sup> were

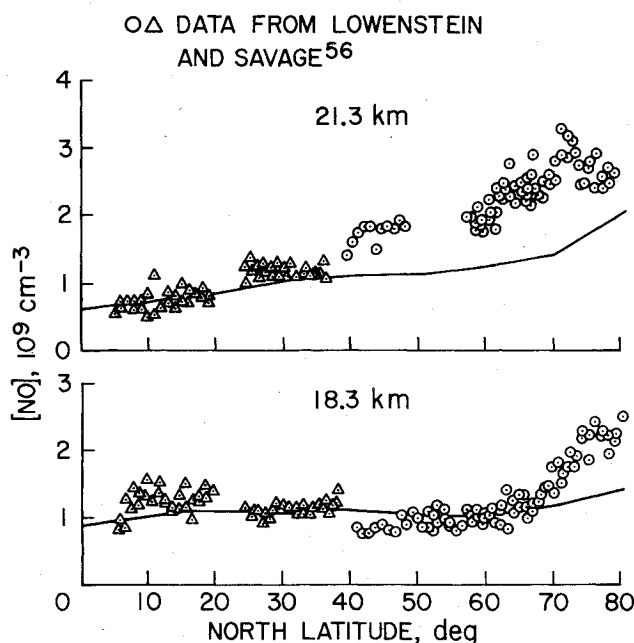


Fig. 9 Nitric oxide number densities vs latitude for two altitudes. The symbols represent the measurements of Loewenstein and Savage.<sup>56</sup> Both the data and calculations are for local noon of a summer season.

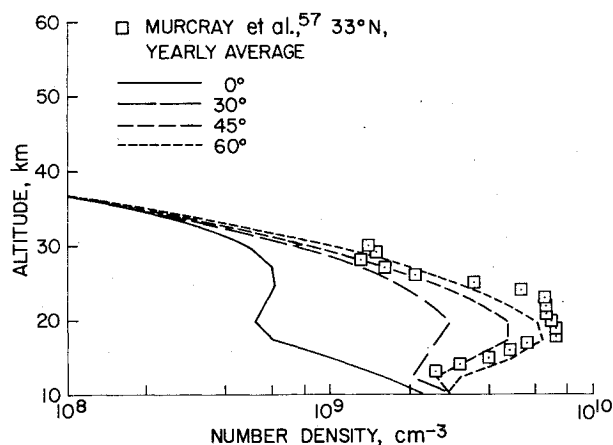


Fig. 10 Calculated vs measured nitric acid ( $\text{HNO}_3$ ) concentration as a function of altitude for four different latitudes. Data are taken from the work of Murcay et al.<sup>57</sup>

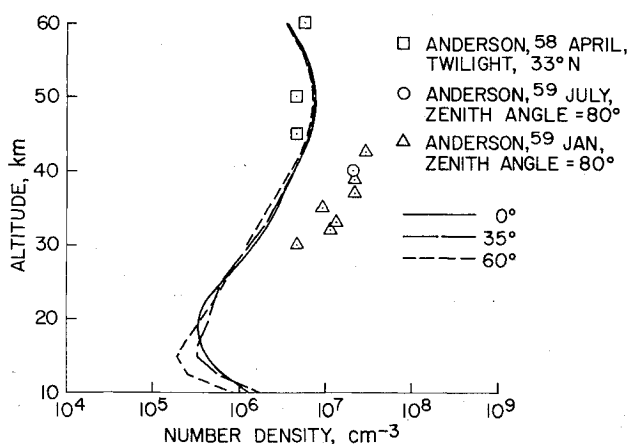


Fig. 11 Calculated vs measured hydroxyl concentrations as a function of altitude for four different latitudes. The measurements are taken from Anderson.<sup>58,59</sup>

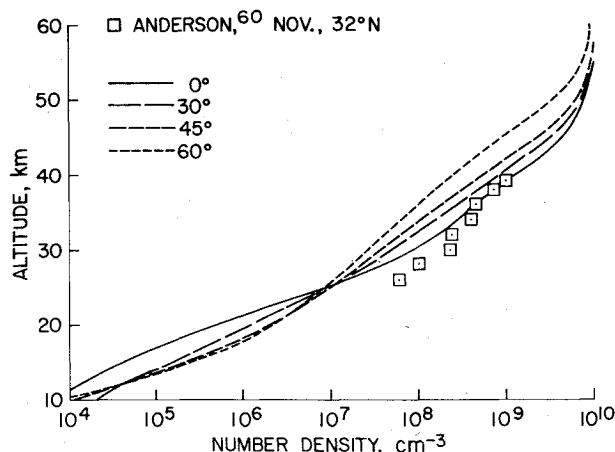


Fig. 12 Calculated vs measured atomic oxygen concentrations as a function of altitude for four different latitudes. The measurements are from Anderson.<sup>60</sup> The calculations for for local noon in the Winter season.

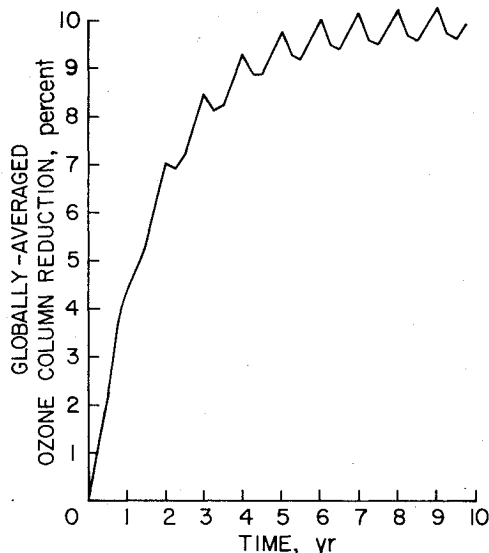


Fig. 13 Globally averaged ozone column reduction as a function of time after initiation of hypothetical SST operations.

used with his wind velocities reduced by a factor of three. However, when these transport coefficients and reduced wind velocities were used to calculate the ozone and other trace species distributions, the ozone distribution was in strong disagreement with the measurements (see Fig. 6). Much better agreement between the measured and predicted ozone distribution is obtained when the unmodified winds and transport coefficients described previously are used (see Fig. 7). This figure shows that the absolute level of ozone is about right and that the predicted value oscillates about the measurements. The local maxima and minima in the predicted curve are evidently due to the use of a set of transport coefficients that is independent of the winds chosen. Hence, the following results must be considered preliminary pending further improvement of the transport parameters.

It should be emphasized here that all of the following results, and those shown in Fig. 7, are based on the winds and transport coefficients described in the section titled "Transport" and are not those of Louis.<sup>54</sup>

The program was run to simulate a period of 10 years, which was sufficient to approach a steady state. Figures 8-12 show the calculated number of densities of  $O_3$ ,  $NO$ ,  $HNO_3$ ,  $OH$ , and  $O(^3P)$  vs altitude for the ambient atmosphere. An examination of the figures shows that our predictions agree

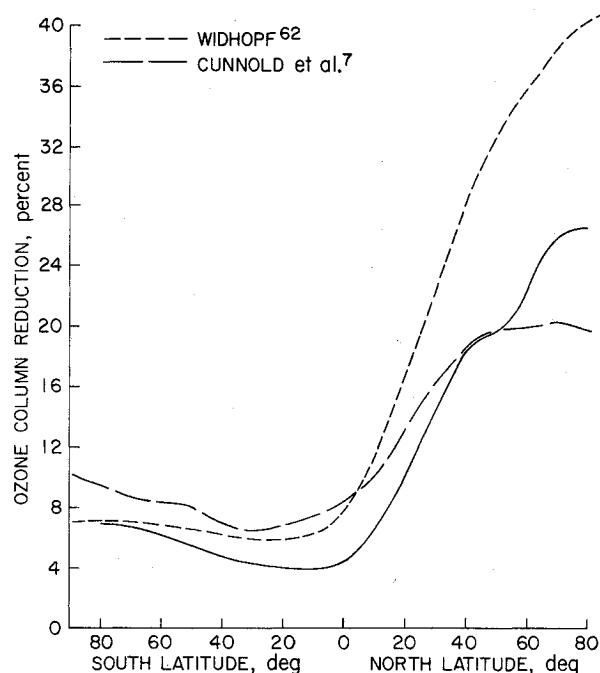


Fig. 14 One year average ozone column reduction as a function of latitude 10 years after commencement of operations.

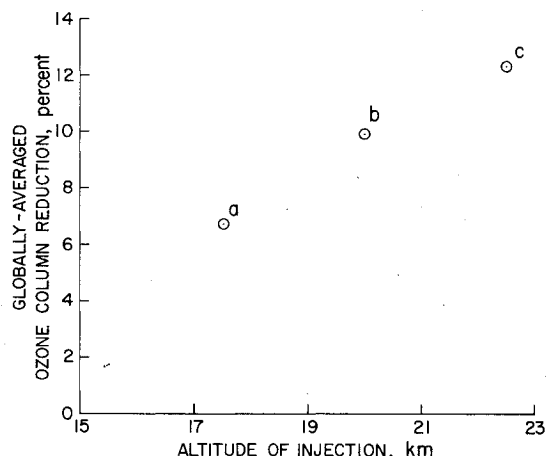


Fig. 15 Globally averaged ozone column density reduction following 10 years of SST operations at three altitudes of flight: a) 17.5 km, b) 20 km, and c) 22.5 km.

reasonably well with the measurements where these are available. Variations of species concentrations with both latitude and season are evident. Having thus demonstrated that the model predicts reasonably well the concentrations of a number of species in the unperturbed stratosphere, we can now investigate some of the effects of aerospace vehicle operations in the stratosphere.

To calculate the perturbation of stratospheric ozone caused by a fleet of SSTs, two computer runs were made: one for the ambient atmosphere and a second run identical to the first except that  $NO_2$  was injected at a rate of  $1.8 \times 10^6$  metric tons\*\* per year at an altitude of 20 km for latitudes between  $40^\circ$  and  $50^\circ N$ .

The calculated reduction in global ozone due to  $NO_2$  injection from a future fleet of supersonic transports vs time is given in Fig. 13. After a 10-year integration time, the reduction has reached 10%. Figure 14 displays the reduction as a function of latitude. The dashed curve in Fig. 14 represents

\*\*This injection rate is equal to that used by Cunnold et al.<sup>7</sup> in their calculations. It represents approximately 1000 advanced SSTs operating 7 hr per day.

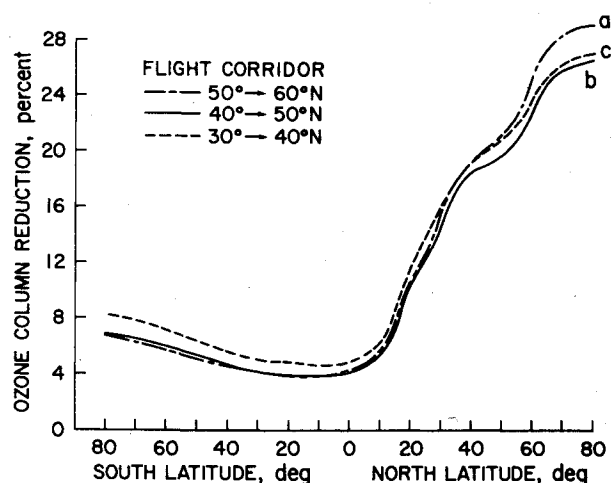


Fig. 16 Calculated ozone column density reductions as a function of latitude for three different flight corridors: a) 50°N-60°N, b) 40°N-50°N, c) 30°N-40°N.

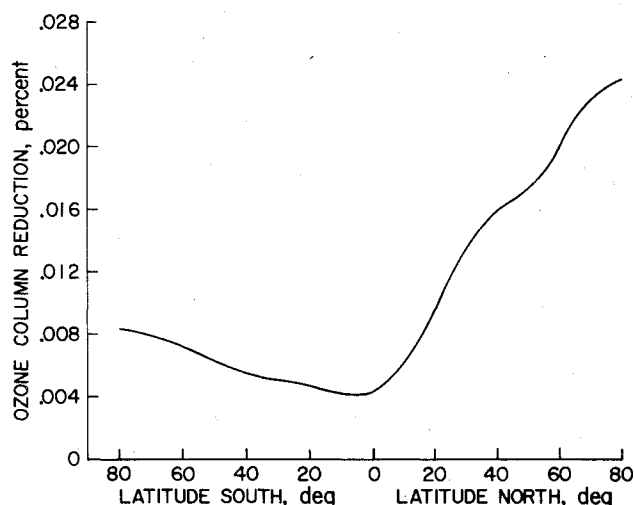


Fig. 17 Calculated ozone column density reduction vs latitude for the Concorde flight schedule listed in Table 3.

the results of a three-dimensional model run from Cunnold et al.<sup>7</sup> for a similar episode of injection. It can be seen from Fig. 14 that our model predicts a latitude-dependent ozone depletion similar in appearance to that given by Cunnold et al.<sup>7</sup> They report a globally averaged ozone depletion of 12% in good agreement with our model prediction of 10% for the same flight frequency and altitude. The results of Widhopf<sup>62</sup> are also shown in Fig. 14. Their results for the Northern Hemisphere are much higher than those of the Ames two-dimensional model and those of Cunnold et al.<sup>7</sup> This difference might be due to their use of winds and transport coefficients that do not vary seasonally. Nevertheless, all three sets of calculations indicate a strong corridor effect in that the predicted ozone depletions are largest to the north of the flight corridor for aircraft operating in the northern hemisphere.

We have also tested the sensitivity of the ozone depletion with respect to SST flights at different altitudes and flight corridors. Figure 15 shows the globally averaged ozone depletion for three different altitudes of flight for 10 years of simulated operations. Clearly our model predicts increased ozone depletions at higher flight altitudes. In Fig. 16 we show the effects due to different flight corridors. It can be seen that the latitude dependence of the ozone column depletion is relatively insensitive to the flight corridors chosen in this simulation.

Table 3 Flight schedule and emission characteristics for the British-French Concorde<sup>61</sup>

Flight schedule:		
London 52° N, 0° to Bahrain 25° N, 52° E		4/week
London 52° N, 0° to New York 41° N, 74° W		14/week
Paris 49° N, 2-1/2° E to New York 41° N, 74° W		14/week
London 52° N, 0° to Washington 38° N, 77-1/2° W		14/week
Paris 49° N, 2-1/2° E to Washington 38° N, 77-1/2° W		14/week
Paris 49° N, 2-1/2° E to Rio 21° S, 41° W		2/week
Bahrain 25° N, 52° E to Singapore 2° N, 104° E		3/week
Singapore 2° N, 104° E to Melbourne 38° S, 145° E		3/week
Emission characteristics:		
Speed	2130 km/hr	
Altitude	{ 15 km first 2/3 of flight 17-1/2 km last 1/3 of flight	
NO <sub>2</sub> emission	340 kg/hr NO <sub>2</sub>	

We stress here that the previous discussion regarding the effects of SST operations in the stratosphere is appropriate for the standard problem of 1000 supersonic transports operating 7 hr per day. A fleet of such magnitude is not anticipated in the near future. A more realistic assessment of the potential effects of SST operations on stratospheric ozone can be obtained by considering the current British-French Concorde flight schedule. Assuming the flight emission characteristics given in Table 3, we have again run our model as described above to simulate a period of 10 years. A careful comparison of Figs. 16 and 17 shows that there is *relatively* more ozone reduction in the Southern Hemisphere than in the Northern Hemisphere for the Concorde case. This is to be expected because the Concorde flight schedule calls for flights in the Southern Hemisphere as well as in the Northern Hemisphere. The globally averaged ozone reduction was then found to be 0.01%, a value three decades lower than that obtained from the hypothetical fleet of 1000 flights/day. However, before we can regard our estimates as definitive, the transport of trace species in the atmosphere must be better understood and documented, and the model modified accordingly.

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